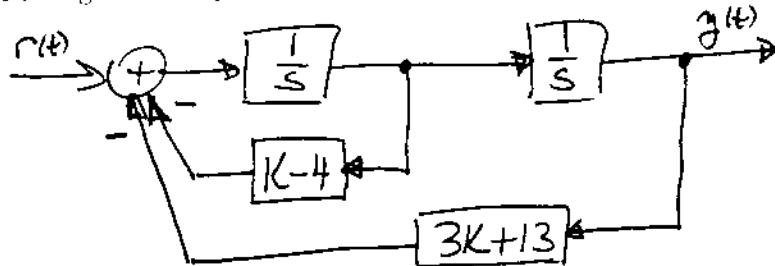


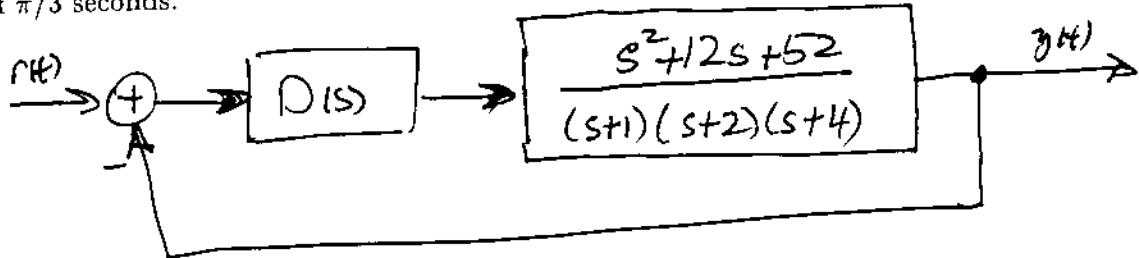
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1. Consider the following control system.

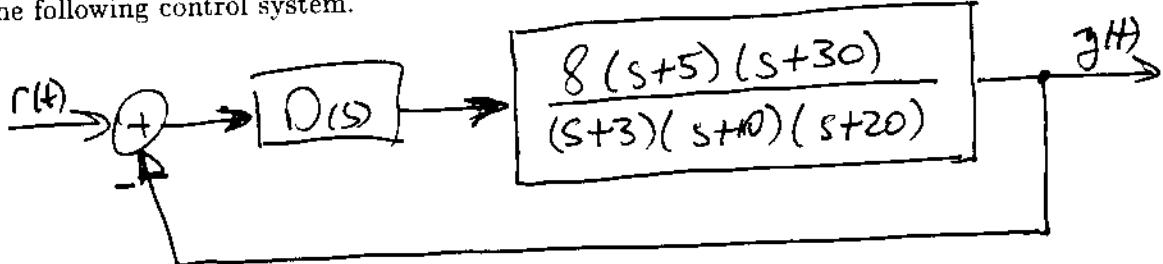


- (a) Construct the root-locus diagram as K goes from 0 to ∞ . (15pts)
 (b) Construct the root-locus diagram as K goes from 0 to $-\infty$. (15pts)
 (c) Determine the range of K for the asymptotical stability of the closed-loop system. (15pts)

2. For the following system, design a first order compensator $D(s)$, without increasing the order of the system, such that the dominant complex poles would produce a 5% settling time of 1.5 seconds and a peak time of $\pi/3$ seconds. (35pts)



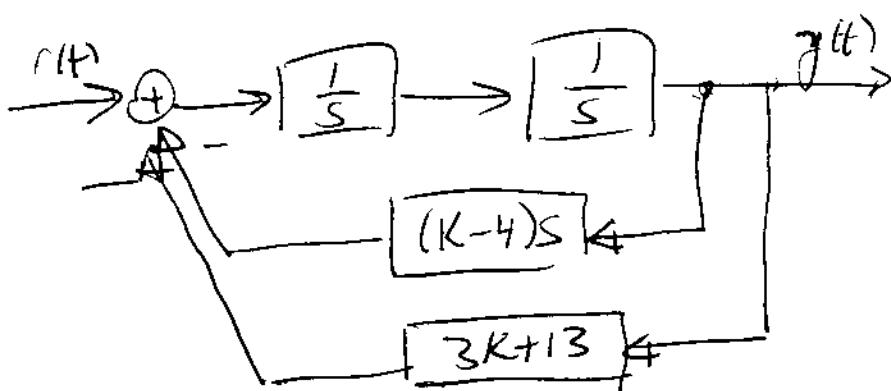
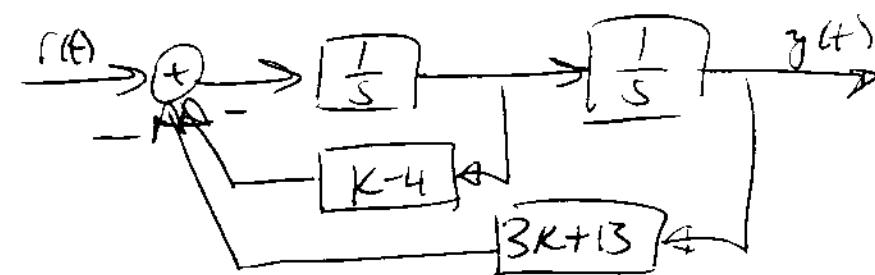
3. Consider the following control system.



- (a) Design a compensator $D(s)$, such that the steady state error, $e(\infty)$ is zero for a step input, and it is 0.1 for the unit ramp input. (20pts)
 (b) Design a compensator $D(s)$, such that the steady state error, $e(\infty)$ is zero for a ramp input. (+20pts)

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#1



$$\Rightarrow G(s) = \frac{1}{s^2}, \quad H(s) = (K-4)s + (3K+13)$$

$$1+GH = 1 + \frac{(K-4)s + (3K+13)}{s^2} = 0$$

$$s^2 + (K-4)s + (3K+13) = 0$$

$$s^2 + Ks - 4s + 3K + 13 = 0$$

$$s^2 - 4s + 13 + Ks + 3K = 0$$

$$(s^2 - 4s + 13) + K(s+3) = 0$$

$$1 + K \frac{s+3}{s^2 - 4s + 13} = 0$$

So the new open-loop gain is $G'H' = K \frac{s+3}{s^2 - 4s + 13}$

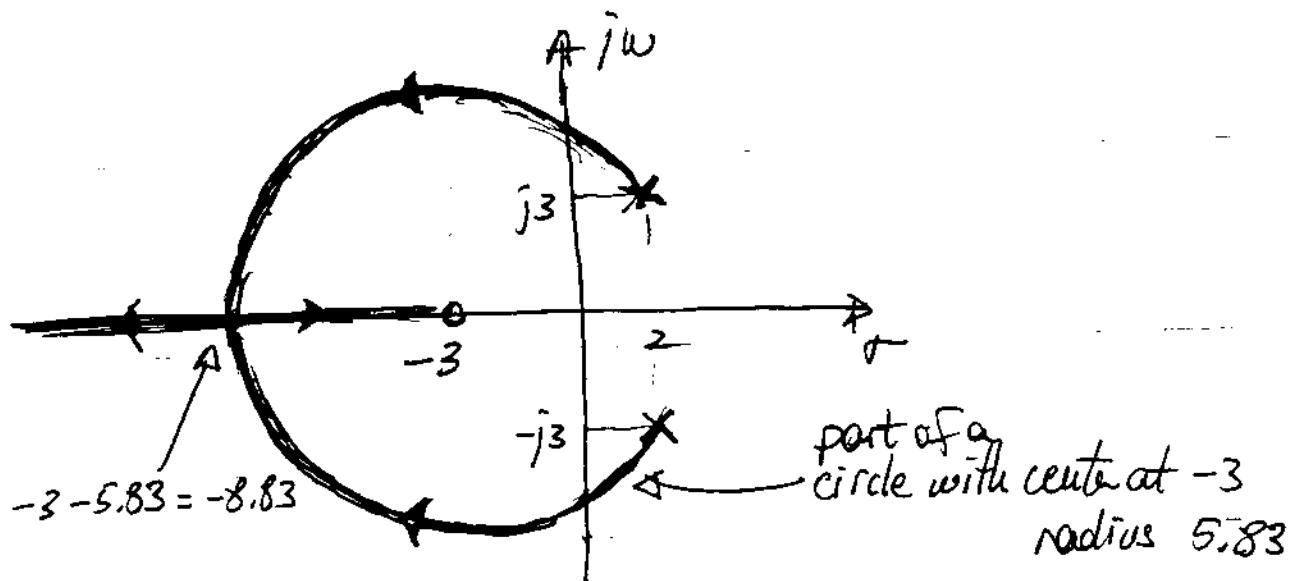
s.t. the original gain GH and the new gain $G'H'$ give the same closed-loop poles. So let's use the new gain for root-loops.

$$Q_H \quad K > 0 \quad G'H' = K \frac{s+3}{s^2 - 4s + 13} \quad \begin{matrix} \leftarrow \\ \leftarrow \end{matrix}$$

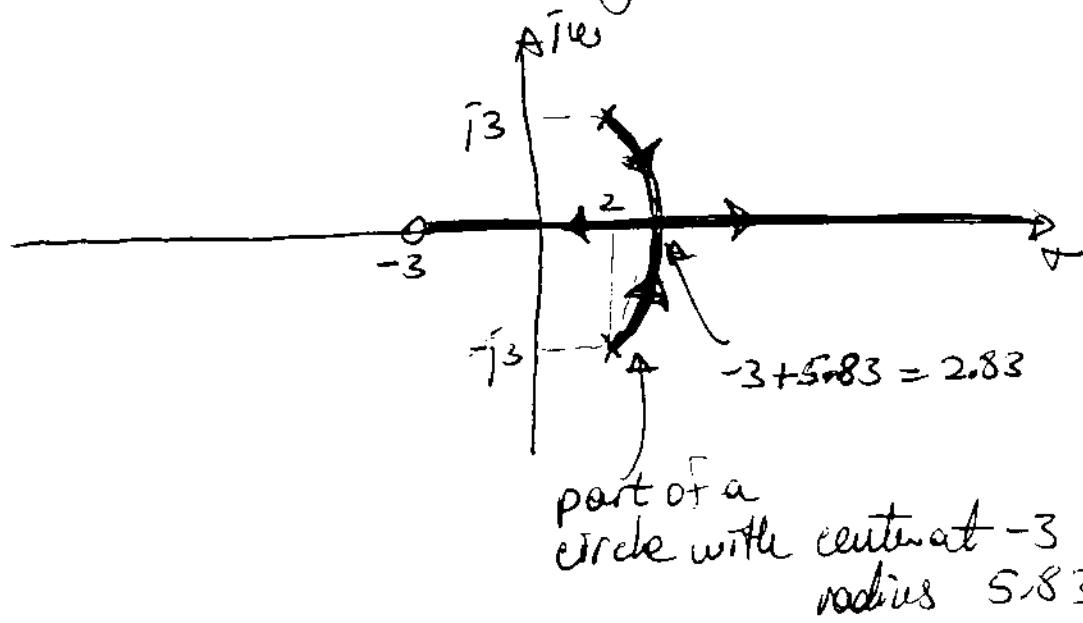
$s_{1,2} = +2 \pm j3 \quad \begin{matrix} \nearrow \\ \nearrow \end{matrix}$ two poles & one zero

\Rightarrow root-loops is part of a circle with center at the zero or $s = -3$ and radius $r = \sqrt{(p_1 - z)(p_2 - z)}$

$$\begin{aligned} &= \sqrt{(+2 + j3 - (-3))(-2 - j3 - (-3))} \\ &= \sqrt{(5 + j3)(5 - j3)} \\ &= \sqrt{5^2 + 3^2} = \sqrt{34} \approx 5.83 \end{aligned}$$



b) $K < 0$ The root-loops in this case will be the remaining portion of the circle



c) The best way to determine the range of K for asymptotical stability is to use Routh table

The closed-loop poles satisfy

$$1 + G_H = 0 \text{ or from previous analysis}$$

$$s^2 + (K-4)s + (3K+13) = 0$$

$$\begin{array}{c|cc} s^2 & 1 & 3K+13 \\ s & K-4 & \implies K-4 > 0, K > 4 \\ 1 & 3K+13 & \implies 3K+13 > 0, 3K > -13, K > -\frac{13}{3} \end{array}$$

so $K > 4$
and
 $K > -\frac{13}{3}$

$$\implies \boxed{K > 4}$$

#2 $D(s)$ s.t. $t_{5\%s} = 1.5$

$$t_p = \frac{\pi}{3}$$

For dominant complex poles $t_{5\%s} = \frac{3}{T_0}$

$$\Rightarrow 1.5 = \frac{3}{T_0} \Rightarrow T_0 = 2$$

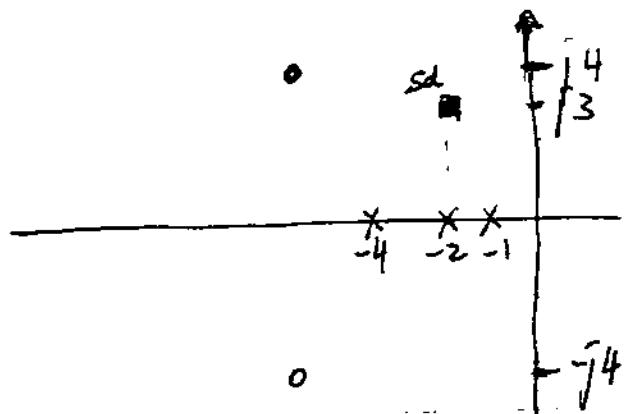
$$t_p = \frac{\pi}{\omega_d}$$

$$\Rightarrow \frac{\pi}{3} = \frac{\pi}{\omega_d} \Rightarrow \omega_d = 3$$

\Rightarrow desired closed-loop poles are at

$$s_d = -2 \pm j3$$

$$G_H = D(s) \frac{s^2 + 12s + 52}{(s+1)(s+2)(s+4)} \quad s_1 = -6 \pm j4$$

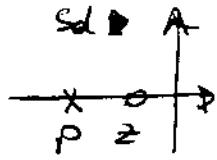


So the angle needed for the root locus going through s_d is

$$\begin{aligned} \phi &+ \tan^{-1} \frac{3-4}{-2-(-6)} + \tan^{-1} \frac{3-(-4)}{-2-(-6)} - \tan^{-1} \frac{3-0}{-2-(-1)} \\ &- \tan^{-1} \frac{3-0}{-2-(-2)} - \tan^{-1} \frac{3-0}{-2-(-4)} = (2k+1) 180^\circ \end{aligned}$$

$$\phi + (-14.04^\circ) + 60.26^\circ - 108.43^\circ - 90^\circ \\ - 56.31^\circ = (2k+1)180^\circ$$

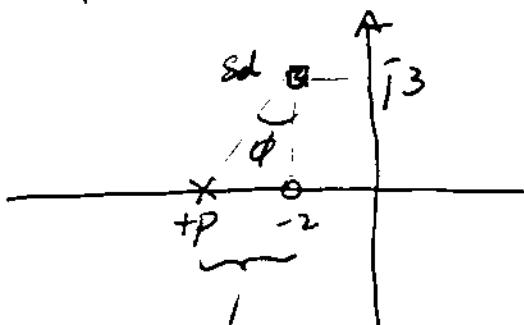
$\phi = 28.53^\circ \Rightarrow$ Design a lead compensator

$$\hookrightarrow D(s) = K \frac{s+z}{s-p}$$


In order not to increase the system order, the lead compensator should cancel one of the poles and place another pole.

One possible pole to cancel is at $s = -2$, i.e. $z = -2$

so



$$\hookrightarrow 3 \tan \phi = 3 \tan 28.53^\circ = 1.63$$

$$\Rightarrow p = -2 - 1.63 = -3.63$$

$$\text{or } D(s) = K \frac{s+2}{s+3.63}$$

To find K , we need to use the magnitude condition

$$\left| G H \right|_{s=s_d} = 1 \quad \text{or} \quad \left| K \frac{s+z}{s+p} \cdot \frac{s^2 + 12s + 52}{(s+1)(s+2)(s+4)} \right|_{s=-2+j3} = 1$$

$$\Rightarrow K = 1.17 \quad \text{or} \quad D(s) = 1.17 \frac{s+2}{s+3.63}$$

#3

$$G_H = D(s) \frac{8(s+5)(s+30)}{(s+3)(s+10)(s+20)}$$

Q1, For $e(\infty) = 0$ for a step input, the system has to be TYPE I or $D(s) = D'(s) \frac{1}{s}$

For $e(\infty) = 0.1$ for unit ramp input, we first need to find K_V , assuming $D'(s) = K$

$$K_V = \lim_{s \rightarrow 0} s G_H = \lim_{s \rightarrow 0} s K \frac{8(s+5)(s+30)}{s(s+3)(s+10)(s+20)} \\ = 2K \Rightarrow e(\infty) = \frac{1}{K_V} = \frac{1}{2K}$$

Requirement $e_{\text{desired}}(\infty) = 0.1$

$$\Rightarrow \frac{1}{2K} = 0.1 \quad \text{or} \quad K = 5$$

So if $D(s) = \frac{5}{s}$ keeps the system stable, we are successful. We can check the stability using

Routh criterion

Closed-loop poles $1 + GH = 0$

$$1 + \frac{40(s+5)(s+30)}{s(s+3)(s+10)(s+20)} = 0$$

$$s(s+3)(s+10)(s+20) + 40(s+5)(s+30) = 0$$

$$s^4 + 33s^3 + 330s^2 + 2000s + 6000 = 0$$

$\sqrt{6}s^4$	1	330	6000
$\sqrt{6}s^3$	33	2,000	
$\sqrt{6}s^2$	$330 - \frac{2000}{33} = 269.39$	6,000	
$\sqrt{6}s$	$2000 - \frac{33 \times 6000}{269.39} = 1,265.02$		
$\sqrt{6}$	6,000		

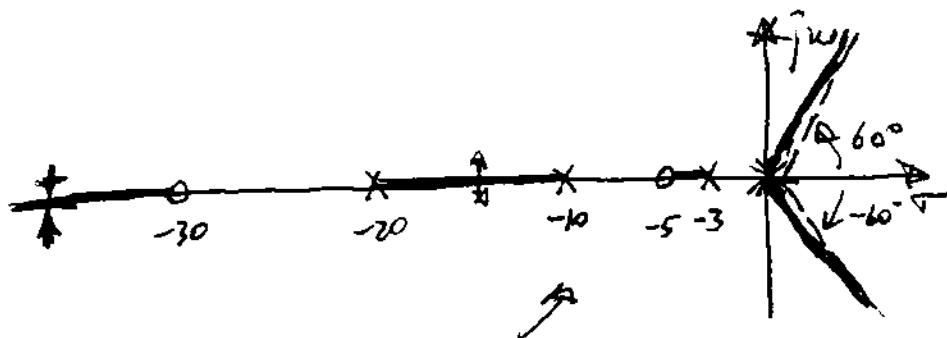
So the system is stable and $D(s) = \frac{5}{s}$
is acceptable.

b) For $e(\infty) = 0$ for unit ramp, we need

$$D(s) = D'(s) \frac{1}{s^2}$$

$$\text{so } GHT = D'(s) \frac{8(s+5)(s+30)}{s^2(s+3)(s+10)(s+20)}$$

Unfortunately, in this case $D'(s) = K$ does not give a stable system since from the rough sketch of the root locus plot, we get



$$\text{Asymptotes } \tau_a = \frac{\sum p_i - \sum z_i}{n-m} = \frac{0+0+(-3)+(-10)+(-20)-(-5)+(-3)}{5-2} = \frac{2}{3}$$

$$\theta_a = \frac{(2k+1)180^\circ}{n-m} = \frac{(2k+1)180^\circ}{5-2} = \pm 60^\circ, 120^\circ$$

The two poles at $s=0$, immediately becomes unstable for any gain (even for the open-loop). As a result, we conclude that we need more dynamics in the compensator. At this point, we have two choices

① add more poles \rightarrow a bad idea, since it would decrease θ_a (but would probably move τ_a s.t. $\tau_a < 0$)

② add zeros \rightarrow a better idea, since we can easily add two zeros to the compensator, and it would still be proper.

\rightarrow add one zero \rightarrow bad idea since it would increase θ_a

\rightarrow add two zeros \rightarrow a good idea

One possibility is to add complex zeros so that the poles leaving $s=0$ would go towards these zeros

so let the zeros be at $s = -4 \pm j^4$

i.e. $D(s) = K \frac{s^2 + 8s + 32}{s^2}$

Here any $K > 0$ would work.