#### Porosity-Permeability Relations in Granular, Fibrous and Tubular Geometries

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# Outline

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- Permeability of tubular and granular geometries
- Permeability and drag force of fibrous geometries
- Summary

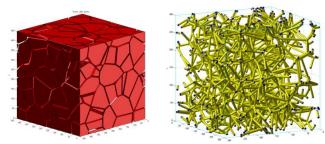


# Motivations

- Porosity-permeability relations for idealized geometries are important guide to understand the porosity-permeability relations of real porous media
- Porosity-permeability relation in porous media with spherical particles is well-understood (Camen-Kozeny equation<sup>1</sup>)

$$k = \frac{\varepsilon d^2}{180(1-\varepsilon)^2}$$
  $d$  – diameter;  $\varepsilon$  – porosity

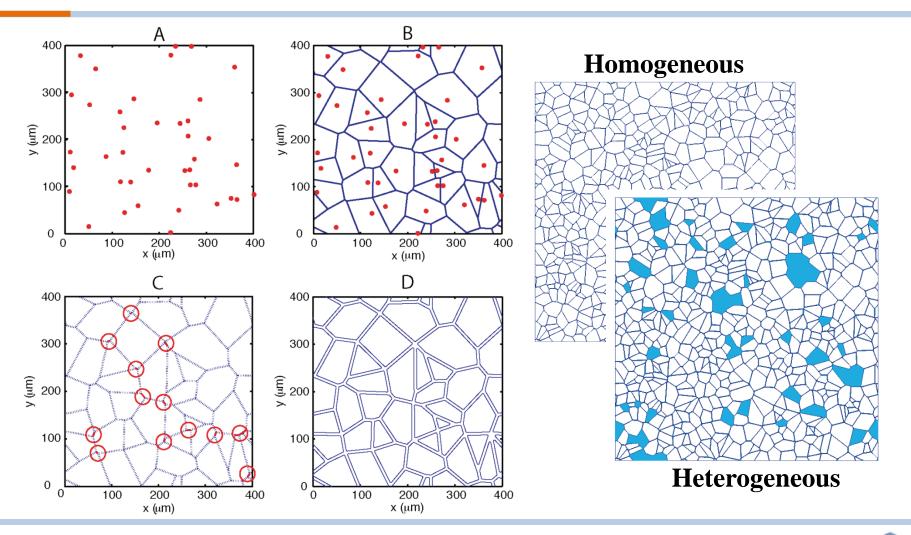
- Geometries with angular grains (henceforthly mentioned as "granular"), tubular and fibrous porous media requires more understanding
- Voronoi diagram will be used to create idealized granular, tubular and fibrous geometry models, and porosity-permeability data will be presented







#### Stochastic porous media geometries

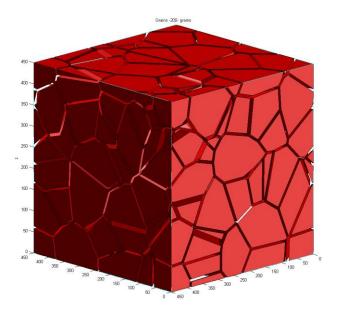


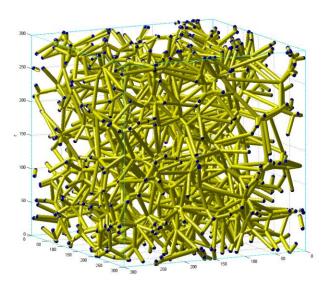


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#### Stochastic porous media geometries

• Angular grains – "Granular" • Tubular/Fibrous



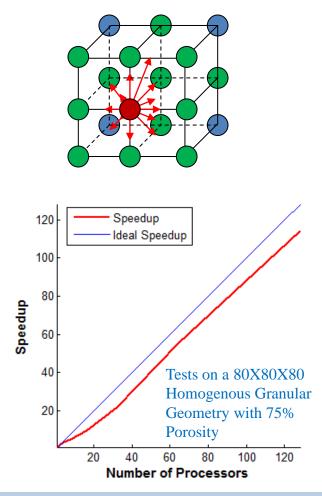






### Lattice Boltzmann method

- Propagation model
  - D3Q19: 3 dimensional, 19 velocities
- Collision model
  - MRT Multi-Relaxation Time for both shear and bulk viscosities, improved accuracy and stability
- Boundary condition
  - Bounce back on solid walls
- Parallel computing simulator
  - Nearly ideal speedup up to 128 processes
  - Largest system simulated contains
    ~1.3 billion voxels (fluid and solid)
- Simulation input parameters
  - Body force density 0.0001, 0, 0
  - Tau (Shear)
  - Tau\_v (Bulk )

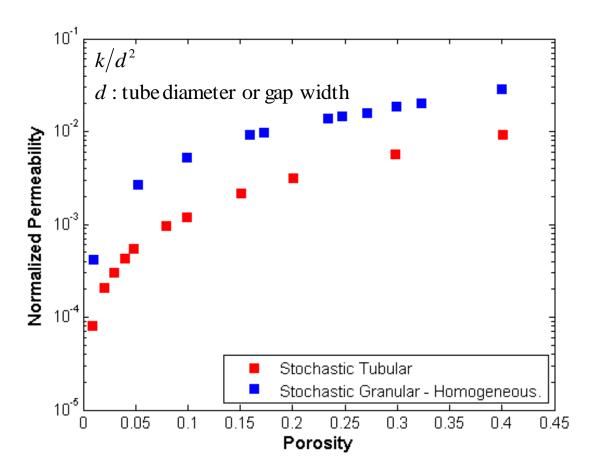


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#### Permeability of granular and tubular geometries

- Porosity-permeability relations established using the "obvious" length scales (gap and tube size) are qualitatively similar
- Granular (fractured) geometries have higher normalized permeabilities







#### Permeability of granular and tubular geometries

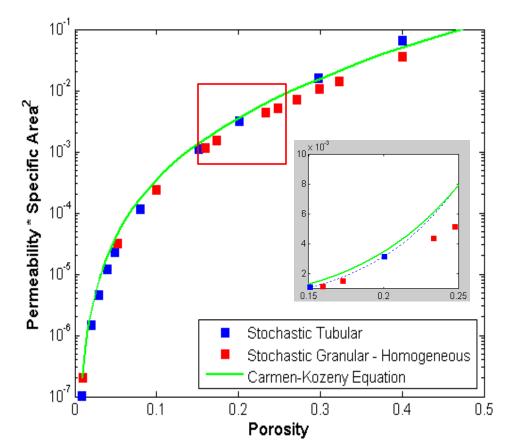
 Carman-Kozeny equation uses (specific surface area)<sup>-1</sup> as the length scale

 $s = \frac{\text{surface area}}{\text{solid volume}}$ 

• When specific surface area is used, granular an tubular data are close

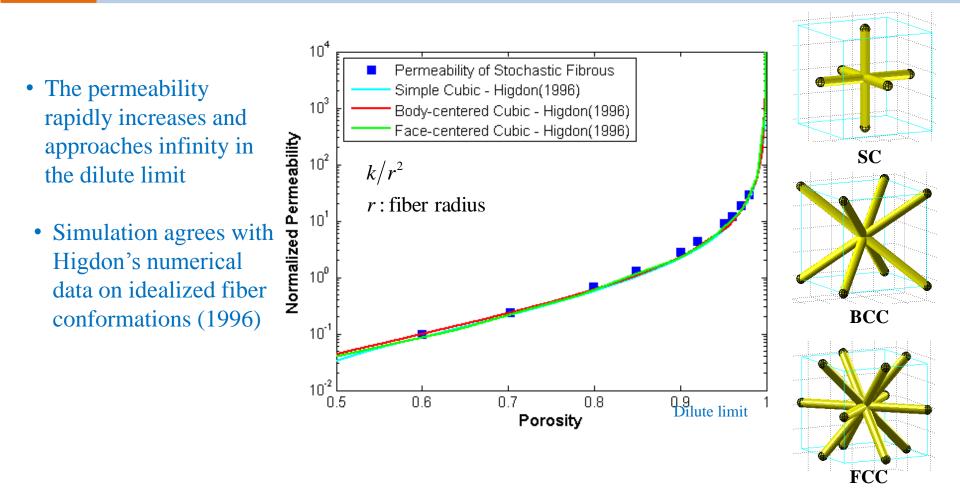
$$ks^2 = \frac{C\varepsilon^3}{(1-\varepsilon)^2}$$
 C = 2.5 for tubes

- When ε > 0.15, normalized tubular permeability is higher than normalized granular permeability
- When ε < 0.15, the difference is very small</li>





### Permeability of fibrous geometries

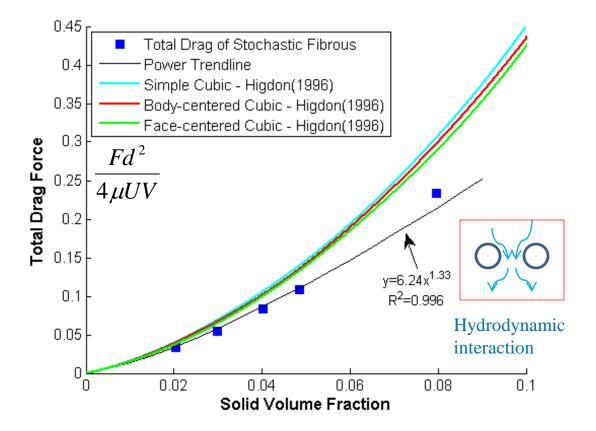






### Permeability of fibrous geometries: total drag

- Hydrodynamic interaction in the fibrous geometry is indicated by a power index of 1.33
- Greater deviation from Higdon (1996) at higher solid volume fraction is due to the difference in the structure: lower coordination number in our geometry models than in SC/BCC/FCC





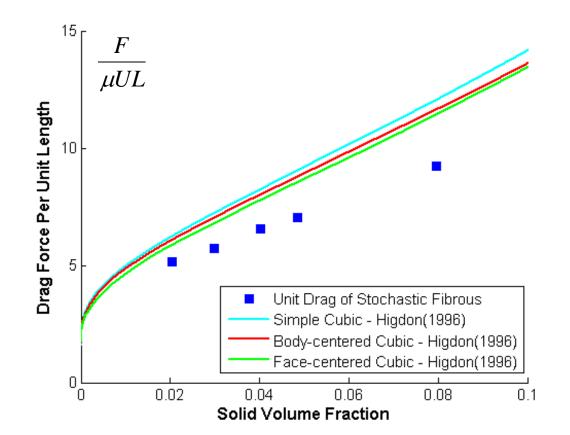


### Drag force per unit length of fibers

• Effective fiber length

 $L = 4V_s / \pi d^2$ 

- Hydrodynamic interaction is still significant in the dilute limit
- Higdon's data show rapid decrease in the drag force per unit length in the dilute limit, consistent with theories
- We plan to run more simulations in the dilute limit to study the scaling of the drag force



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## Summary

- Permeability normalized using specific surface area are close between granular and tubular geometries
- At high porosity (>0.15), tubular geometry is more permeable than homogeneous granular geometry
- Fibrous geometry simulation results shows a rapid increase of permeability in the dilute limit
- The effect of hydrodynamic interaction in our geometry model is weaker than in SC/BCC/FCC models (Higdon, 1996)

#### Acknowledgement

- RPSEA
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