$\qquad$

1. (4 points) A hollow aluminum shaft with an outside diameter of 100 mm and a wall thickness of 5 mm has an allowable shear stress of 40 MPa . Determine the maximum torque $T$ that may be applied to the shaft.
2. (6 points) A solid constant-diameter shaft is subjected to the torques shown. The bearings shown allow the shaft to turn freely. Determine the internal torque in segments (1), (2), and (3) of the shaft. Use the sign convention presented in class and Section 6-6 of the text.

3. (6 points) In the gear system shown, the motor applies a torque of 250 N - m to the gear at A . The bearings shown allow free rotation of the shafts. Determine the internal torque magnitude in shafts (1) and (2).

4. (6 points) In the gear system shown, the motor rotates at 21 Hz . Determine the rotation speed magnitude of shafts (1) and (2).

5. (7 points) The drive shaft of an automobile is being designed to transmit 280 hp at $3,500 \mathrm{rpm}$. Determine the minimum diameter required for a solid steel shaft if the allowable shear stress in the shaft is not to exceed 4,000 psi.
6. (8 points) The compound shaft shown consists of aluminum segment (1) and steel segment (2). Aluminum segment (1) is a tube with an outside diameter of $D_{1}=4.00 \mathrm{in}$., a wall thickness of $t_{1}=0.25 \mathrm{in}$., and a shear modulus of $G_{1}=4,000 \mathrm{ksi}$. Steel segment (2) is a tube with an outside diameter of $D_{2}=2.50 \mathrm{in}$., a wall thickness of $t_{2}=0.125 \mathrm{in}$., and a shear modulus of $G_{2}=12,000 \mathrm{ksi}$. The compound shaft is subjected to torques applied at $B$ and $C$. Determine the rotation angle of $C$ with respect to the support at $A$. Use the sign convention presented in class and Section 6-6 of the text.

7. (10 points) The composite shaft shown consists of a solid brass segment (1) and a solid aluminum segment (2) that are connected at flange B and securely attached to rigid walls at A and C. Brass segment (1) has a diameter of 18 mm and a shear modulus of 39 GPa . Aluminum segment (2) has a diameter of 24 mm , and a shear modulus of 28 GPa . If a concentrated torque of 270 N -m is applied to flange B, determine the torque magnitude in segments (1) and (2).

8. (5 points) The dimensions of the shape are shown. Determine the centroid location measured from the bottom of the shape.

9. (12 points) Use the graphical method to construct the shear-force and bending-moment diagrams for the beam shown. Label all significant points on the diagram, and identify the maximum moment(s) along with the respective location(s). Clearly distinguish straight-line and curved portions of the diagrams.

10. ( 8 points) The dimensions of the shape are shown. The centroid is 15.59 inches from the bottom of the shape. Determine the moment of inertia about the $z$ axis.

11. (12 points) A composite beam is made of two brass [ $\mathrm{E}=100 \mathrm{GPa}$ ] plates bonded to an aluminum [ $\mathrm{E}=75$ GPa] bar. The beam is subjected to a bending moment of $1,750 \mathrm{~N}-\mathrm{m}$ acting about the z axis. Determine the maximum bending stress magnitude in the brass plates.

12. (6 points) A WT305 $\times 41$ standard steel shape is subjected to a tension force $\mathrm{P}=134.9 \mathrm{kN}$ that is applied 250 mm above the bottom surface of the tee shape. Using the attached table, determine the following items.


The vertical distance from the bottom surface to the centroid of the tee shape $=$ $\qquad$ mm

The moment of inertia that would be relevant to this problem = $\qquad$ $\mathrm{mm}^{4}$
$\qquad$ Nm
13. (10 points) The tee shape is used as a post that supports a load of $\mathrm{P}=25 \mathrm{kN}$. Note that the load P is applied 400 mm from the flange of the tee shape. The centroid is 49 mm left of point K , and the moment of inertia around the $z$ axis is $10,761,666.67 \mathrm{~mm}^{4}$. Determine the normal stresses at point H .



Shapes Cut from Wide-Flange Sections or WT Shapes

| Designation | Area A | Depth $d$ | Web thickness $t_{w}$ | Flange width $b_{f}$ | Flange thickness $t_{f}$ | Centroid $\bar{y}$ | $I_{x}$ | $S_{x}$ | $\boldsymbol{r}_{\boldsymbol{x}}$ | $I_{y}$ | $S_{y}$ | $r_{y}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | in. ${ }^{2}$ | in. | in. | in. | in. | in. | in. ${ }^{4}$ | in. ${ }^{3}$ | in. | in. ${ }^{4}$ | in. ${ }^{3}$ | in. |
| WT12×47 | 13.8 | 12.2 | 0.515 | 9.07 | 0.875 | 2.99 | 186 | 20.3 | 3.67 | 54.5 | 12.0 | 1.98 |
| WT12×38 | 11.2 | 12.0 | 0.440 | 8.99 | 0.680 | 3.00 | 151 | 16.9 | 3.68 | 41.3 | 9.18 | 1.92 |
| WT12 $\times 34$ | 10.0 | 11.9 | 0.415 | 8.97 | 0.585 | 3.06 | 137 | 15.6 | 3.70 | 35.2 | 7.85 | 1.87 |
| WT12×27.5 | 8.10 | 11.8 | 0.395 | 7.01 | 0.505 | 3.50 | 117 | 14.1 | 3.80 | 14.5 | 4.15 | 1.34 |
| WT10.5 $\times 34$ | 10.0 | 10.6 | 0.430 | 8.27 | 0.685 | 2.59 | 103 | 12.9 | 3.20 | 32.4 | 7.83 | 1.80 |
| WT10.5 $\times 31$ | 9.13 | 10.5 | 0.400 | 8.24 | 0.615 | 2.58 | 93.8 | 11.9 | 3.21 | 28.7 | 6.97 | 1.77 |
| WT10.5 $\times 25$ | 7.36 | 10.4 | 0.380 | 6.53 | 0.535 | 2.93 | 80.3 | 10.7 | 3.30 | 12.5 | 3.82 | 1.30 |
| WT10.5 $\times 22$ | 6.49 | 10.3 | 0.350 | 6.50 | 0.450 | 2.98 | 71.1 | 9.68 | 3.31 | 10.3 | 3.18 | 1.26 |
| WT $9 \times 27.5$ | 8.10 | 9.06 | 0.390 | 7.53 | 0.630 | 2.16 | 59.5 | 8.63 | 2.71 | 22.5 | 5.97 | 1.67 |
| WT9 $\times 25$ | 7.33 | 9.00 | 0.355 | 7.50 | 0.570 | 2.12 | 53.5 | 7.79 | 2.70 | 20.0 | 5.35 | 1.65 |
| WT9 $\times 20$ | 5.88 | 8.95 | 0.315 | 6.02 | 0.525 | 2.29 | 44.8 | 6.73 | 2.76 | 9.55 | 3.17 | 1.27 |
| WT $9 \times 17.5$ | 5.15 | 8.85 | 0.300 | 6.00 | 0.425 | 2.39 | 40.1 | 6.21 | 2.79 | 7.67 | 2.56 | 1.22 |
| WT8 $\times 28.5$ | 8.39 | 8.22 | 0.430 | 7.12 | 0.715 | 1.94 | 48.7 | 7.77 | 2.41 | 21.6 | 6.06 | 1.60 |
| WT8 $\times 25$ | 7.37 | 8.13 | 0.380 | 7.07 | 0.630 | 1.89 | 42.3 | 6.78 | 2.40 | 18.6 | 5.26 | 1.59 |
| WT8 $\times 20$ | 5.89 | 8.01 | 0.305 | 7.00 | 0.505 | 1.81 | 33.1 | 5.35 | 2.37 | 14.4 | 4.12 | 1.56 |
| WT $8 \times 15.5$ | 4.56 | 7.94 | 0.275 | 5.53 | 0.440 | 2.02 | 27.5 | 4.64 | 2.45 | 6.2 | 2.24 | 1.17 |
|  | $\mathrm{mm}^{2}$ | mm | mm | mm | mm | mm | $\begin{gathered} 10^{6} \\ \mathrm{~mm}^{4} \end{gathered}$ | $\begin{gathered} 10^{3} \\ \mathrm{~mm}^{3} \end{gathered}$ | mm | $\begin{gathered} 10^{6} \\ \mathrm{~mm}^{4} \end{gathered}$ | $\begin{gathered} 10^{3} \\ \mathrm{~mm}^{3} \end{gathered}$ | mm |
| WT305×70 | 8900 | 310 | 13.1 | 230 | 22.2 | 75.9 | 77.4 | 333 | 93.2 | 22.7 | 197 | 50.3 |
| WT305×56.5 | 7230 | 305 | 11.2 | 228 | 17.3 | 76.2 | 62.9 | 277 | 93.5 | 17.2 | 150 | 48.8 |
| WT305 $\times 50.5$ | 6450 | 302 | 10.5 | 228 | 14.9 | 77.7 | 57.0 | 256 | 94.0 | 14.7 | 129 | 47.5 |
| WT305 $\times 41$ | 5230 | 300 | 10.0 | 178 | 12.8 | 88.9 | 48.7 | 231 | 96.5 | 6.04 | 68.0 | 34.0 |
| WT265 $\times 50.5$ | 6450 | 269 | 10.9 | 210 | 17.4 | 65.8 | 42.9 | 211 | 81.3 | 13.5 | 128 | 45.7 |
| WT265×46 | 5890 | 267 | 10.2 | 209 | 15.6 | 65.5 | 39.0 | 195 | 81.5 | 11.9 | 114 | 45.0 |
| WT265×37 | 4750 | 264 | 9.65 | 166 | 13.6 | 74.4 | 33.4 | 175 | 83.8 | 5.20 | 62.6 | 33.0 |
| WT265 $\times 33$ | 4190 | 262 | 8.89 | 165 | 11.4 | 75.7 | 29.6 | 159 | 84.1 | 4.29 | 52.1 | 32.0 |
| WT230 $\times 41$ | 5230 | 230 | 9.91 | 191 | 16.0 | 54.9 | 24.8 | 141 | 68.8 | 9.37 | 97.8 | 42.4 |
| WT230×37 | 4730 | 229 | 9.02 | 191 | 14.5 | 53.8 | 22.3 | 128 | 68.6 | 8.32 | 87.7 | 41.9 |
| WT230×30 | 3790 | 227 | 8.00 | 153 | 13.3 | 58.2 | 18.6 | 110 | 70.1 | 3.98 | 51.9 | 32.3 |
| WT230×26 | 3320 | 225 | 7.62 | 152 | 10.8 | 60.7 | 16.7 | 102 | 70.9 | 3.19 | 42.0 | 31.0 |
| WT205 $\times 42.5$ | 5410 | 209 | 10.9 | 181 | 18.2 | 49.3 | 20.3 | 127 | 61.2 | 8.99 | 99.3 | 40.6 |
| WT205 $\times 37.5$ | 4750 | 207 | 9.65 | 180 | 16.0 | 48.0 | 17.6 | 111 | 61.0 | 7.74 | 86.2 | 40.4 |
| WT205 $\times 30$ | 3800 | 203 | 7.75 | 178 | 12.8 | 46.0 | 13.8 | 87.7 | 60.2 | 5.99 | 67.5 | 39.6 |
| WT205 $\times 23.05$ | 2940 | 202 | 6.99 | 140 | 11.2 | 51.3 | 11.4 | 76.0 | 62.2 | 2.58 | 36.7 | 29.7 |

