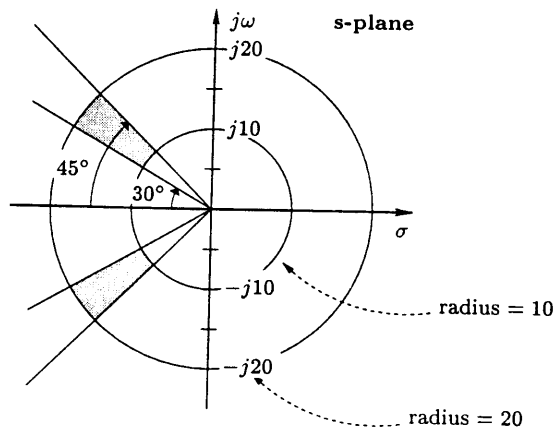
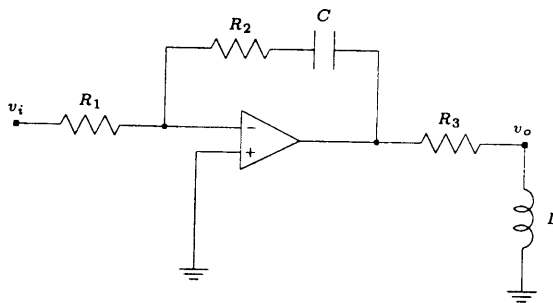


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- Obtain the necessary inequalities to describe the strictly complex poles in the shaded region below in terms of only ζ and ω_n of a second-order system described by $Y(s)/U(s) = \omega_n^2 / (s^2 + 2\zeta\omega_n s + \omega_n^2)$. (20pts)

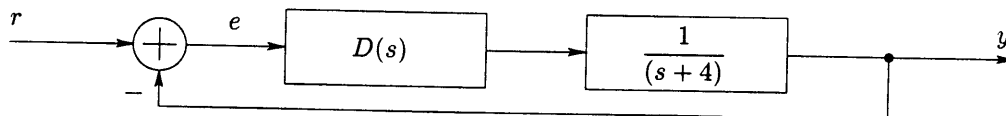


- Consider the following control system.

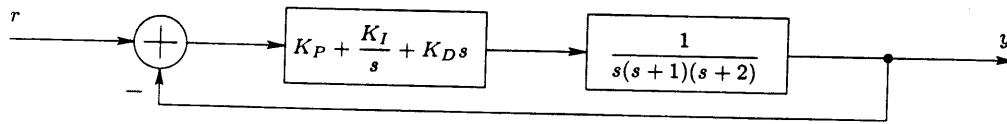


Assume that $R_1 = 1\Omega$, $R_2 = 2\Omega$, $R_3 = 4\Omega$, $C = 1\text{F}$, and $L = 2\text{H}$. Only the capacitor and the inductor are sensitive to temperature changes; such that the sensitivity of the capacitance with respect to temperature $S_T^C = 5$, and the sensitivity of the inductance with respect to temperature $S_T^L = 4$. Determine the sensitivity of the transfer function $V_o(s)/V_i(s)$ with respect to the temperature. (20pts)

- Design the simplest controller $D(s)$, such that the steady-state error for a unit-step reference input is zero, and the maximum percent overshoot is about 10%. Show all your work clearly. (15pts)



4. A PID controller is to be designed for the following control system.



- (a) Determine the requirements for the PID constants K_P , K_I , and K_D , such that the closed-loop system is asymptotically stable. (15pts)
- (b) Determine whether or not the values $K_P = 1$, $K_I = 0$, and $K_D = 1$ result in an asymptotically-stable system. (05pts)

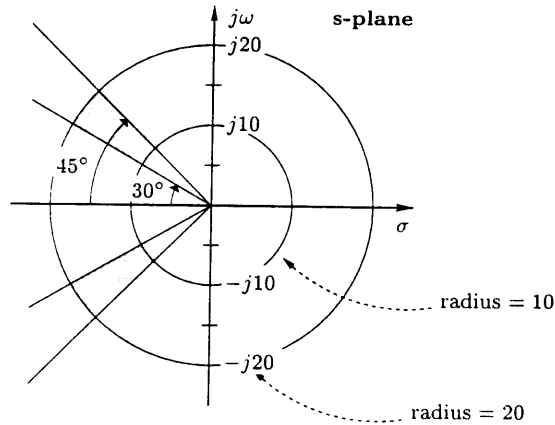
5. Consider a negative unity-feedback control system with the open-loop transfer function

$$G(s) = K \frac{s+1}{(s-1)s(s^2+4s+16)} = K \frac{s+1}{s^4+3s^3+12s^2-16s}$$

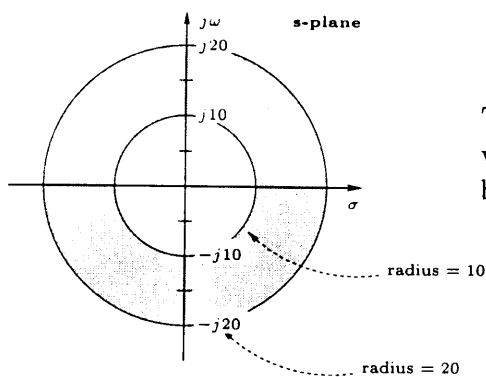
- (a) Determine the values of K such that the closed-loop system is asymptotically stable. (15pts)
- (b) Determine the value (or values) of K and the natural frequency (or frequencies), such that the closed-loop system would have sustained oscillations. (10pts)

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- Obtain the necessary inequalities to describe the strictly complex poles in the shaded region below in terms of only ζ and ω_n of a second-order system described by $Y(s)/U(s) = \omega_n^2 / (s^2 + 2\zeta\omega_n s + \omega_n^2)$.

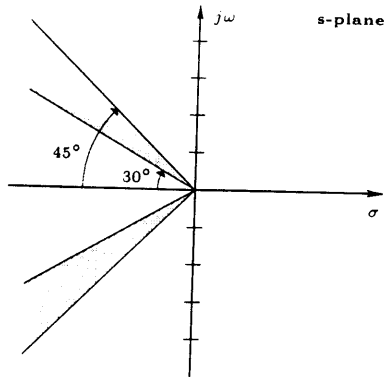


Solution: To be able to describe the shaded region, we need to separate it into unions or intersections of simpler regions.



The equi-distance points from the origin designate constant value for ω_n . As a result, the shown shaded area is represented by

$$10 \leq \omega_n \leq 20.$$



A straight line originating from the origin designates a constant ζ value, where $\cos^{-1}(\zeta)$ is the acute angle between the line and the negative real axis. So for the shaded area shown, we have

$$30^\circ \leq \cos^{-1}(\zeta) \leq 45^\circ,$$

or

$$\cos(30^\circ) \geq \zeta \geq \cos(45^\circ),$$

since $\cos(\theta)$ is a monotonically decreasing function for $0 < \theta < 180^\circ$. So, we have

$$\frac{\sqrt{2}}{2} \leq \zeta \leq \frac{\sqrt{3}}{2}.$$

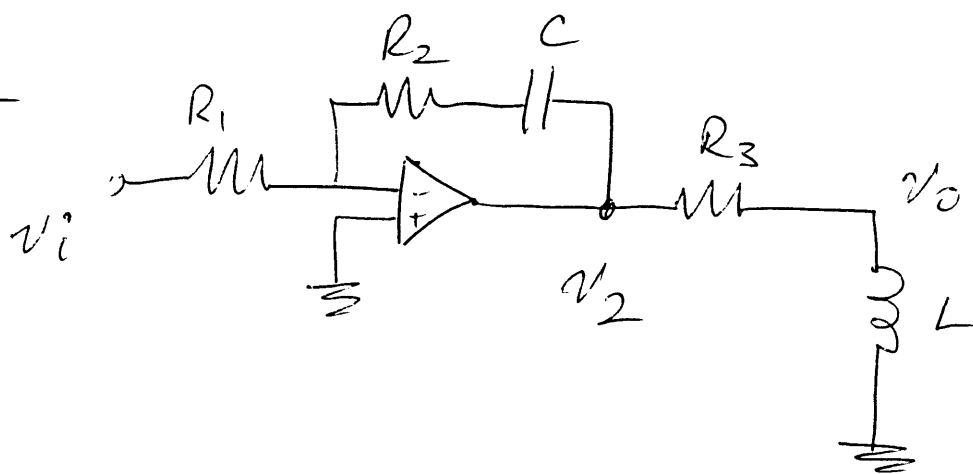
Therefore, the shaded area given in the problem is the intersection of the individual shaded areas, and it can be represented by

$$10 \leq \omega_n \leq 20,$$

$$\frac{\sqrt{2}}{2} \leq \zeta \leq \frac{\sqrt{3}}{2}.$$

(3)

#2



Ideal opamp $\Rightarrow \frac{v_2}{v_i} = - \frac{R_2 + 1/Cs}{R_1}$

Voltage division $\Rightarrow \frac{v_o}{v_2} = \frac{Ls}{R_3 + Ls}$

$$\frac{v_o}{v_i} = \frac{v_o}{v_2} \cdot \frac{v_2}{v_i} = - \left(\frac{R_2}{R_1} + \frac{1}{R_1 C s} \right) \left(\frac{Ls}{Ls + R_3} \right)$$

$$= - \frac{R_2 C s + 1}{R_1 C s} \cdot \frac{Ls}{Ls + R_3} = - \frac{L}{R_1 C} \frac{R_2 C s + 1}{(Ls + R_3)}$$

$$= - \frac{R_2/R_1 s + 1/R_1 C}{s + R_3/L}$$

Sensitivity

$$S_{T}^{v_o/v_i} = S_C^{v_o/v_i} S_T^C + S_L^{v_o/v_i} S_T^L$$

$$S \frac{V_o/V_i}{C} = \frac{C}{V_o/V_i} \frac{\partial (V_o/V_i)}{\partial C}$$

(4)

where

$$\frac{\partial (V_o/V_i)}{\partial C} = - \frac{(-\frac{1}{R_1 C^2})}{s + R_3/L} = \frac{1}{R_1 C^2 (s + R_3/L)}$$

$$\Rightarrow S \frac{V_o/V_i}{C} = \frac{C}{-\frac{(R_2/R_1 s + 1/R_1 C)}{(s + R_3/L)}} \cdot \frac{1}{R_1 C^2 (s + R_3/L)}$$

$$= - \frac{1}{CR_2 s + 1}$$

$$S \frac{V_o/V_i}{L} = \frac{L}{V_o/V_i} \frac{\partial (V_o/V_i)}{\partial L}$$

where

$$\frac{\partial (V_o/V_i)}{\partial L} = - \frac{-(R_2/R_1 s + 1/R_1 C) (-R_3/L^2)}{(s + R_3/L)^2}$$

$$\Rightarrow S \frac{V_o/V_i}{L} = \left(\frac{L}{-\frac{(R_2/R_1 s + 1/R_1 C)}{(s + R_3/L)}} \right) \left(- \frac{-(R_2/R_1 s + 1/R_1 C) (-R_3/L^2)}{(s + R_3/L)^2} \right)$$

$$S_L^{v_o/v_i} = \frac{R_3}{L} \frac{1}{s + R_3/L} = \frac{1}{\frac{L}{R_3}s + 1}$$

(5)

$$\Rightarrow S_T^{v_o/v_i} = - \frac{1}{CR_2s + 1} S_T^e + \frac{1}{\frac{L}{R_3}s + 1} S_T^L$$

$$= - \frac{1}{2s + 1} (5) + \frac{1}{\frac{2}{4}s + 1} (4)$$

$$= - \frac{5}{2s + 1} + \frac{8}{s + 2} = \frac{11s - 2}{(2s + 1)(s + 2)}$$

$$\#3 \quad M_p = 10\% = 0.1 = e^{-\frac{\zeta}{\sqrt{1-\zeta^2}} \pi} \quad (6)$$

$$\Rightarrow \zeta = \frac{|\ln(M_p)|}{\sqrt{\pi^2 + \ln^2(M_p)}} = 0.59$$

$$e_{ss} = 0 \text{ for a step input} \Rightarrow D(s) = \frac{1}{s} D'(s)$$

$$\text{Simplest } D'(s) = K$$

$$\Rightarrow 1 + D(s)G(s) = 0$$

$$1 + \frac{K}{s} \frac{1}{s+4} = 0$$

$$s(s+4) + K = 0$$

$$s^2 + 4s + K = 0$$

For a second-order system with poles at

$$s = -\zeta \omega_n \pm j \sqrt{1-\zeta^2} \omega_n$$

the char. equation is

$$s^2 + 2\zeta \omega_n s + \omega_n^2 = 0$$

Comparing the terms in

(7)

$$s^2 + 4s + K = 0$$

and

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

we get

$$2\zeta\omega_n = 4 \implies \omega_n = \frac{4}{2\zeta} = \frac{4}{2(0.59)}$$
$$\omega_n^2 = K = 3.38$$

so if $K = \omega_n^2 = (3.38)^2$, then we satisfy all the constraints.

$$K = (3.38)^2 = 11.49$$

or

$$D(s) = \frac{11.49}{s}$$

#4

(a) The characteristic equation is

(8)

$$1 + D(s)G(s) = 0$$

$$1 + \frac{K_p s + K_I + K_D s^2}{s} \cdot \frac{1}{s(s+1)(s+2)} = 0$$

or

$$s^2(s+1)(s+2) + K_p s + K_I + K_D s^2 = 0$$

$$s^4 + 3s^3 + (K_D + 2)s^2 + K_p s + K_I = 0$$

R-H table

s^4	1	$K_D + 2$	K_I
s^3	3	K_p	
s^2	$\frac{3K_D + 6 - K_p}{3}$	K_I	
s^1	$\frac{(3K_D + 6 - K_p)K_p - 9K_I}{3K_D + 6 - K_p}$		
1	$3K_I$		

For asymptotical stability

(9)

$$(i) \quad 3K_0 + 6 - K_P > 0$$

$$(ii) \quad (3K_0 + 6 - K_P)K_P - 9K_I > 0$$

$$(iii) \quad K_I > 0$$

(b) For $K_P = 1$, $K_I = 0$, $K_0 = 1$

$$(i) \quad 3(1) + 6 - (1) \stackrel{?}{>} 0$$
$$8 > 0 \quad (\checkmark)$$

$$(ii) \quad (3(1) + 6 - (1))(1) - 9(0) \stackrel{?}{>} 0$$
$$8 > 0 \quad (\checkmark)$$

$$(iii) \quad 0 \stackrel{?}{>} 0 \quad (\times)$$

Not ^{asympt.} stable

Actually, if $K_I = 0$ the order of the system will be reduced.

For the reduced order system, we get (10)

$$1 + (K_p + K_D s) \cdot \frac{1}{s(s+1)(s+2)} = 0$$

$$s(s+1)(s+2) + K_p + K_D s = 0$$

$$s^3 + 3s^2 + (K_D + 2)s + K_p = 0$$

R-H table

s^3	1	$K_D + 2$
s^2	3	K_p
s	$\frac{3(K_D + 2) - K_p}{3}$	
1	K_p	

For ^{asympt.} stability

(11)

$$(i) \quad 3(K_D + 2) - K_P > 0$$

$$3(11 + 2) - 11 > 0 \quad (\checkmark)$$

$$(ii) \quad K_P > 0$$

$$11 > 0 \quad (\checkmark)$$

So system is asympt. stable.

#5 The char. eqn. is

(12)

$$(a) \quad 1 + K \frac{s+1}{s^4 + 3s^3 + 12s^2 - 16s} = 0$$

$$s^4 + 3s^3 + 12s^2 - 16s + Ks + K = 0$$

R-H Table

s^4	1	12	K
s^3	3	$K-16$	
s^2	$\frac{s^2-K}{3}$	K	
s^2	s^2-K	$3K$	
s	$\frac{-K^2+59K-832}{s^2-K}$		
1	$3K$		

Condition

(13)

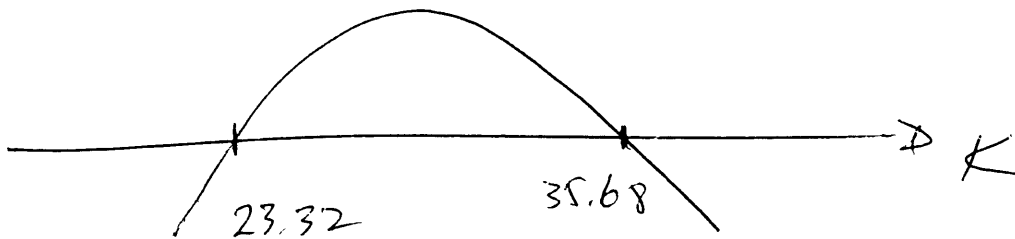
(i)

$$K < 52$$

(ii)

$$-K^2 + 59K - 832 > 0$$

$$-(K - 23.32)(K - 35.68) = 0$$



\Rightarrow

$$23.32 < K < 35.68$$

(iii)

$$K > 0$$

All three cond. are satisfied

iff

$$23.32 < K < 35.68$$

b) Setting a row of zero
(the s-term row)

$$\Rightarrow -K^2 + 59K - 832 = 0$$

$$-(K - 23.32)(K - 35.68) = 0$$

s²-term
↓

When $\boxed{K = 23.32}$ →

$$(52 - K)s^2 + 3K = 0$$

$$\Rightarrow 28.68s^2 + 69.96 = 0$$

$$s = \pm j 1.5618$$

$$\Rightarrow \boxed{\omega = 1.5618}$$

When $\boxed{K = 35.68}$ →

$$(52 - K)s^2 + 3K = 0$$

$$\Rightarrow 16.32s^2 + 107.04 = 0$$

$$s = \pm j 2.5610$$

$$\boxed{\omega = 2.5610}$$