

LECTURE-41

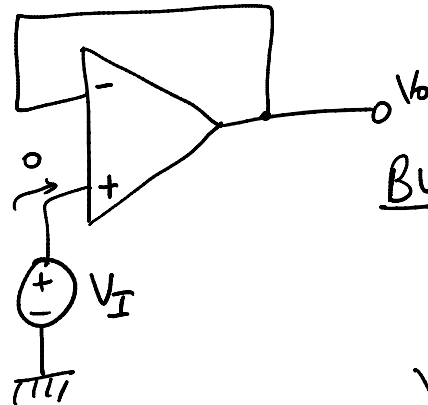
APPLICATION OF NON-INVERTING AMPLIFIER
IS A VOLTAGE FOLLOWER

$$A_v = 1 + \frac{R_2}{R_1}$$

IF R_1 IS $\infty \Omega$ [o.c]

$$A_v = \frac{V_o}{V_i} = 1 \leftarrow \text{UNITY GAIN}$$

SINCE GAIN IS INDEPENDENT OF $R_2 \therefore R_2 = 0$

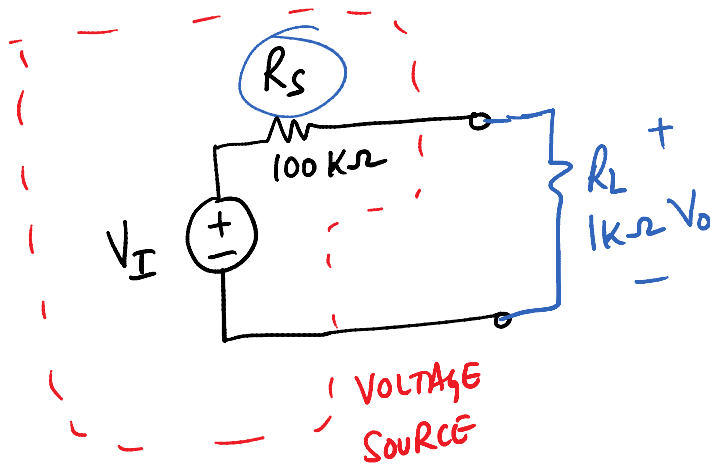


BUFFER

$$R_{in} = \infty \Omega$$
$$R_o = 0 \Omega$$

$$V_o = V_i$$

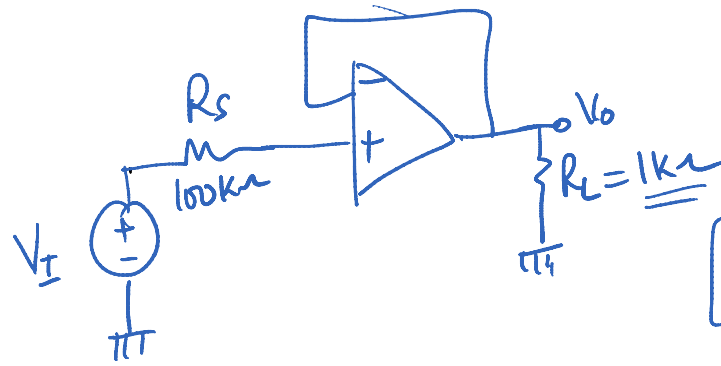
$$A_v = 1$$



$$\frac{V_o}{V_i} = \frac{1k}{1k + 100k} \approx 0.01$$

$$V_o = 0.01 V_i$$

LOADING EFFECT!



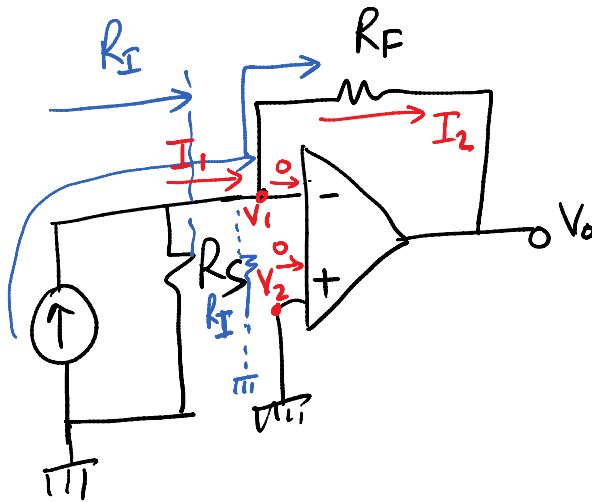
OP-AMP HAS LOW R_o
IDEAL $R_o = 0\Omega$

$$V_o = V_I$$

CURRENT TO VOLTAGE CONVERTER

I TO V CONV.

PHOTODETECTOR → PHOTO DIODE → OUTPUT IS CURRENT



SINCE $V_2 = 0$
 $V_1 = 0$ VIRTUAL GROUND THEORY!

$$R_I = \frac{V_1}{I_1} \approx \underline{\underline{0\Omega}}$$

$$\underline{\underline{R_S \gg R_I}}$$

$$\underline{\underline{I_1 = I_S = I_2}}$$

$$\frac{V_o - V_1}{R_F} = -I_2$$

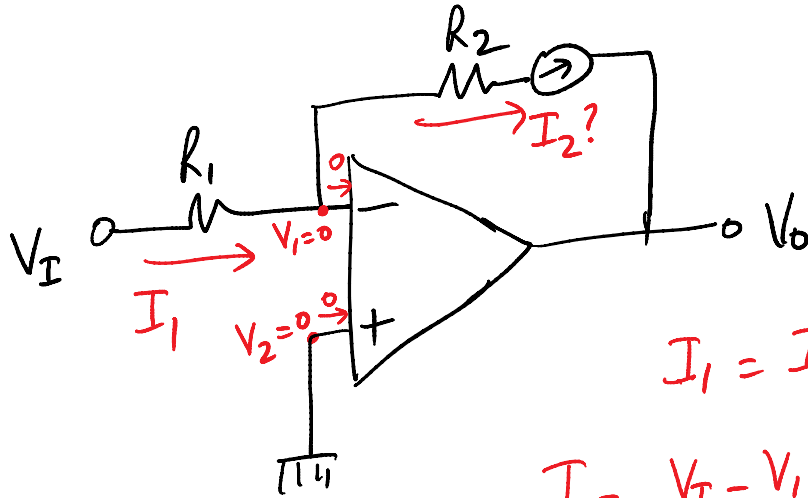
$$V_o = -I_2 R_F$$

$$V_o = -I_S R_F$$

$$V_o \propto I_S$$

V TO I CONVERTER

TO DRIVE A MAGNETIC COIL USING A VOLTAGE SOURCE!



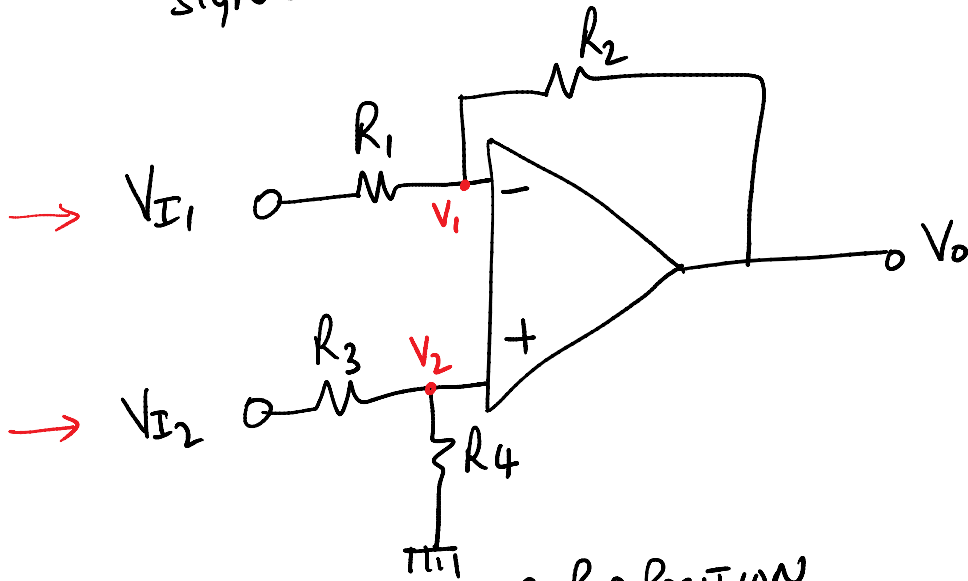
$$I_1 = I_2$$

$$I_1 = \frac{V_I - V_1}{R_1} = \frac{V_I}{R_1}$$

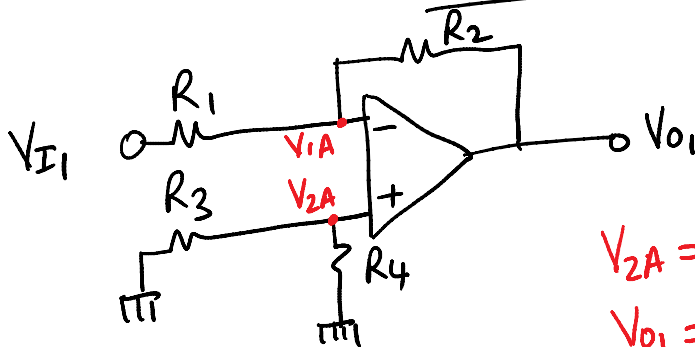
$$I_2 = \frac{V_I}{R_1}$$

DIFFERENCE AMPLIFIER

* AMPLIFIES ONLY THE DIFFERENCE BETWEEN TWO SIGNALS AND REJECTS ANY COMMON SIGNALS TO THE TWO TERMINALS.

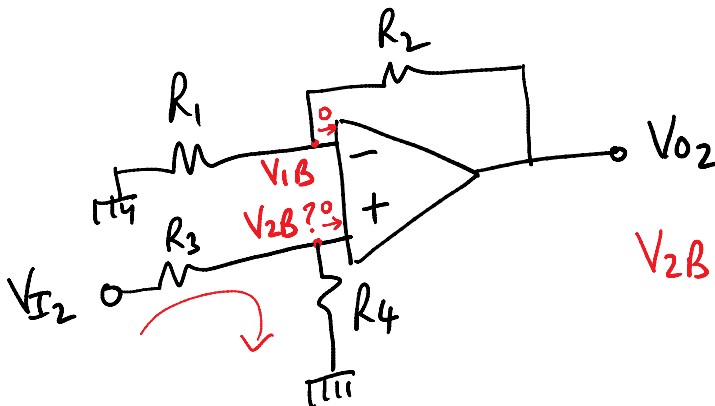


SUPERPOSITION



$$V_{2A} = 0$$

$$V_{O1} = -\frac{R_2}{R_1} (V_{I1}) \dots \textcircled{1}$$



$$V_{2B} = \frac{V_{I2} R_4}{R_3 + R_4}$$

$$V_{1B} = V_{2B} \quad \uparrow \quad \text{NON-INV AMP}$$

$$V_{1B} = V_{2B} \quad \text{---} \quad \text{NOTE}$$

$$V_{O2} = \left(\frac{1+R_2}{R_1} \right) V_{1B} = \left(\frac{1+R_2}{R_1} \right) \left(\frac{R_4}{R_3+R_4} \right) V_{I2} \quad \text{---} \quad \textcircled{2}$$

$$V_O = V_{O1} + V_{O2}$$

$$= \left(\frac{1+R_2}{R_1} \right) \left(\frac{R_4}{R_3+R_4} \right) V_{I2} - \frac{R_2}{R_1} V_{I1}$$

IF $\boxed{\frac{R_4}{R_3} = \frac{R_2}{R_1}}$ DESIGN CRITERIA

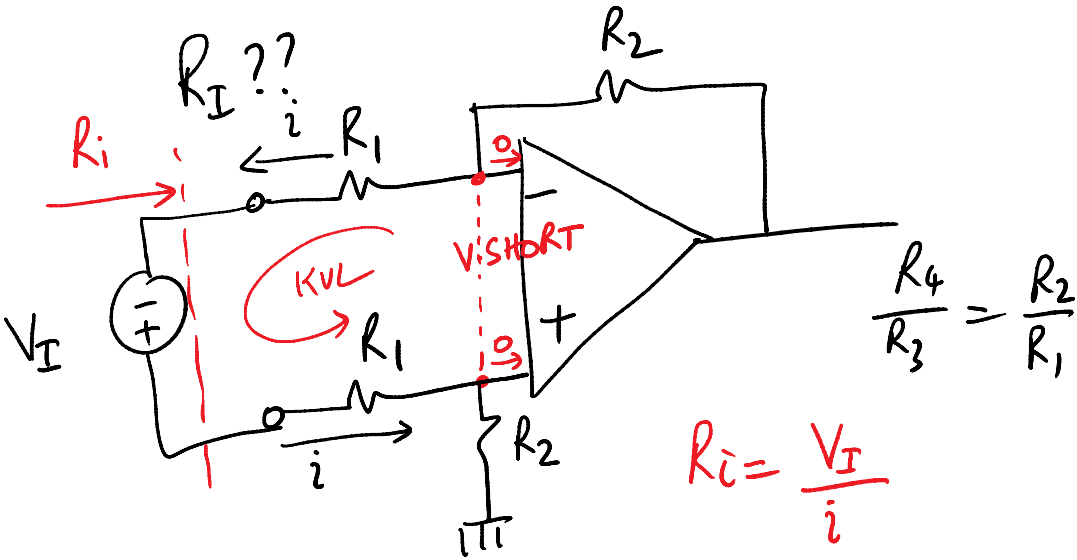
$\therefore \boxed{V_O = \frac{R_2}{R_1} (V_{I2} - V_{I1})}$

NOTE: \rightarrow IF $V_{I2} = V_{I1} \Rightarrow V_O = 0$

Thursday, April 04, 2013
4:15 PM

$$A_d = \frac{V_o}{V_{I2} - V_{I1}} = \frac{R_2}{R_1}$$

CLOSED LOOP
DIFFERENTIAL GAIN



KVL LOOP

$$R_1 i + R_1 i = V_I$$

$$\frac{V_I}{i} = 2R_1$$

Ex

$$\text{GAIN} = 30$$

$$\frac{R_2}{R_1} = \frac{R_4}{R_3} = 30$$

$$R_2 = 30 R_1 \Rightarrow R_2 > R_1$$

IF GAIN TO BE LARGE $\uparrow\uparrow$ $R_1 \downarrow\downarrow$

$$\underline{R_I} = 2 R_1 \downarrow\downarrow$$

\therefore NOT POSSIBLE TO GET HIGH GAIN AND HIGH R_I

* IF $\frac{R_4}{R_3} \neq \frac{R_2}{R_1}$ AND $V_{I_1} = V_{I_2} \Rightarrow$
output $\neq 0$

DEFINE

COMMON MODE INPUT \Rightarrow

$$V_{CM} = \frac{V_{I1} + V_{I2}}{2}$$

$$A_{CM} \rightarrow \text{COMMON MODE GAIN} = \frac{V_o}{V_{CM}}$$

IDEAL CASE $\rightarrow V_o = 0 \Rightarrow A_{CM} = 0$

DEFINE \rightarrow CMRR \rightarrow COMMON MODE REJECTION RATIO

$$= \left| \frac{A_d}{A_{CM}} \right|$$

$$\left(\text{CMRR} \right)_{dB} = 20 \log_{10} \left| \frac{A_d}{A_{CM}} \right|$$

DESIRED $\uparrow\uparrow\uparrow$

Ex $\frac{R_2}{R_1} = 10$ $\frac{R_4}{R_3} = 11$ CMRR??

$$\begin{aligned} V_o &= \left(1 + \frac{R_2}{R_1}\right) \left(\frac{R_4/R_3}{1 + R_4/R_3}\right) V_{I_2} - \frac{R_2}{R_1} V_{I_1} \\ &= (1+10) \left(\frac{11}{1+11}\right) V_{I_2} - 10 V_{I_1} \\ &= 10.0833 V_{I_2} - 10 V_{I_1} \end{aligned}$$

$\left. \begin{aligned} V_d &= V_{I_2} - V_{I_1} \\ V_{CM} &= \frac{V_{I_1} + V_{I_2}}{2} \end{aligned} \right\} \text{SOLVE}$

$V_{I_1} = V_{CM} - \frac{V_d}{2}$

$V_{I_2} = V_{CM} + \frac{V_d}{2}$

$$V_o = 10.0833 \left(V_{CM} + \frac{V_d}{2}\right) - 10 \left(V_{CM} - \frac{V_d}{2}\right)$$

$$V_o = 10.042 V_d + 0.0833 V_{CM} \quad \leftarrow \text{COMPARE}$$

$V_o = A_d V_d + A_{CM} V_{CM}$

$$A_d = 10.042$$

$$A_{CM} = 0.0833$$

$$(CMRR)_{dB} = 20 \log_{10} \left(\frac{10.042}{0.0833}\right) = 41.6dB$$